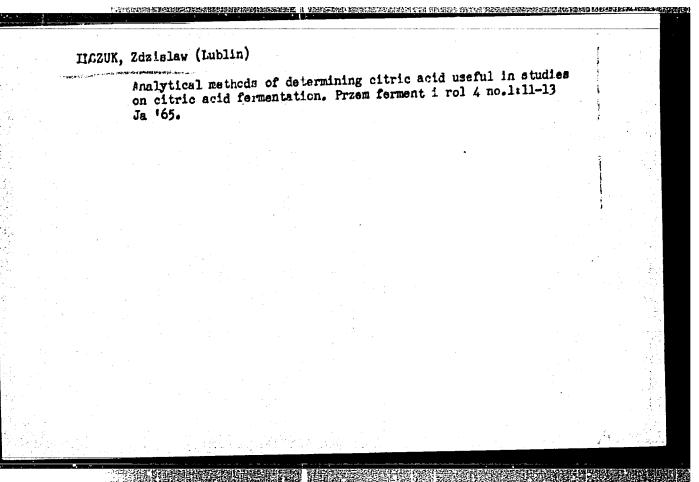
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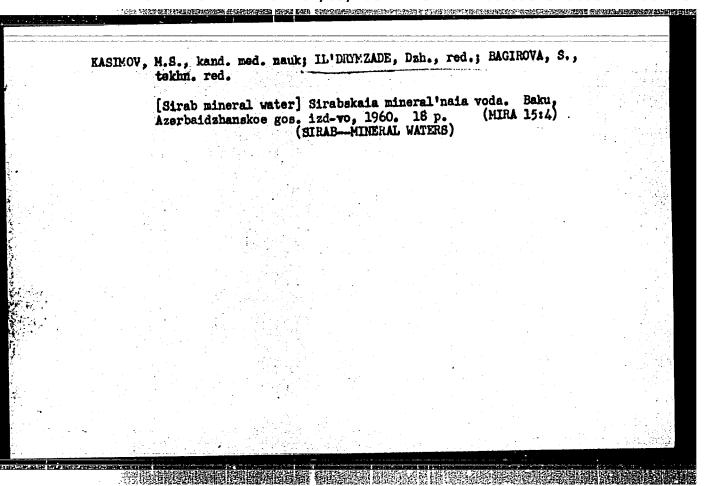
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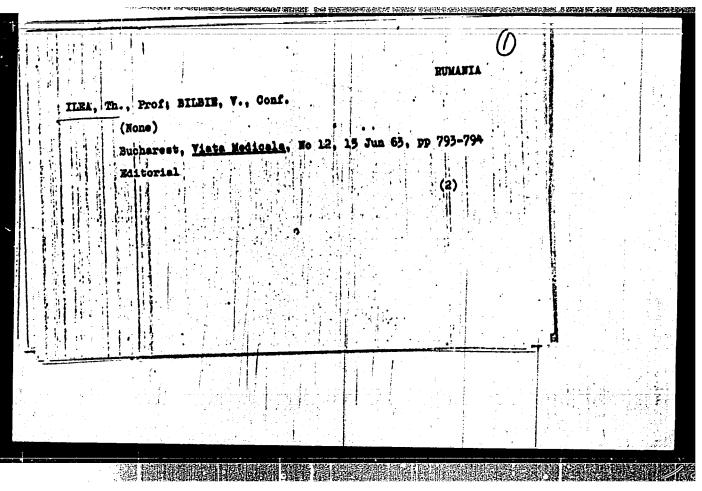
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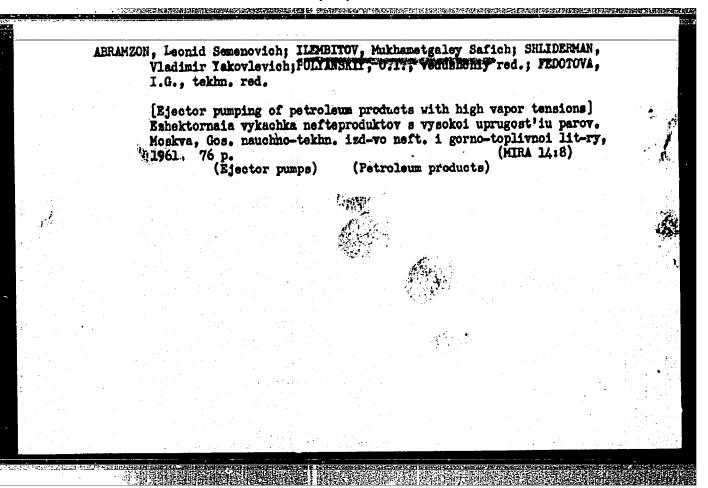
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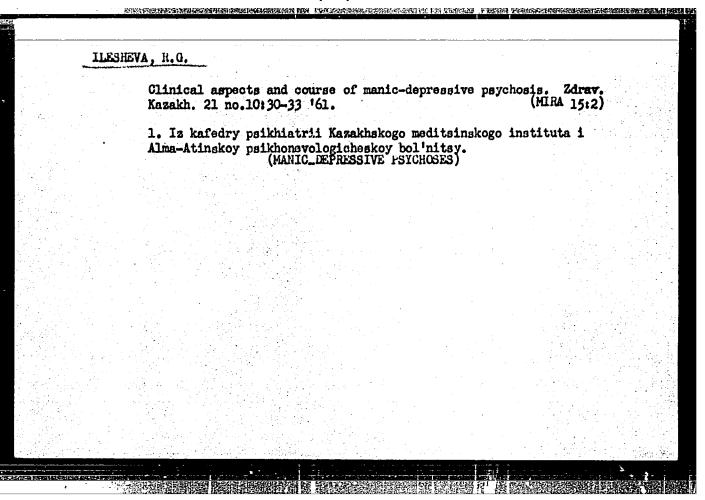
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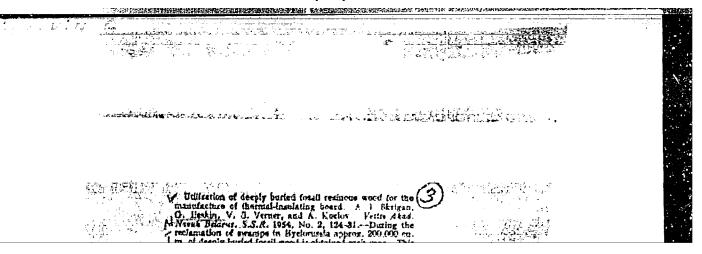
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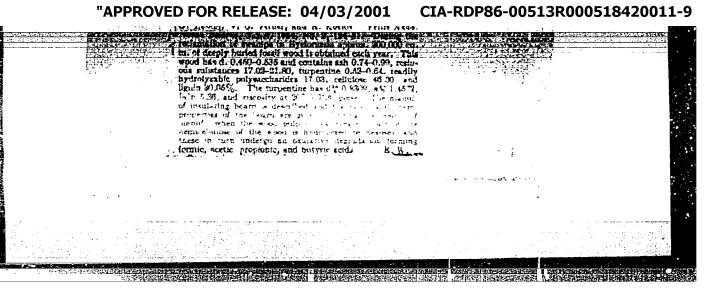
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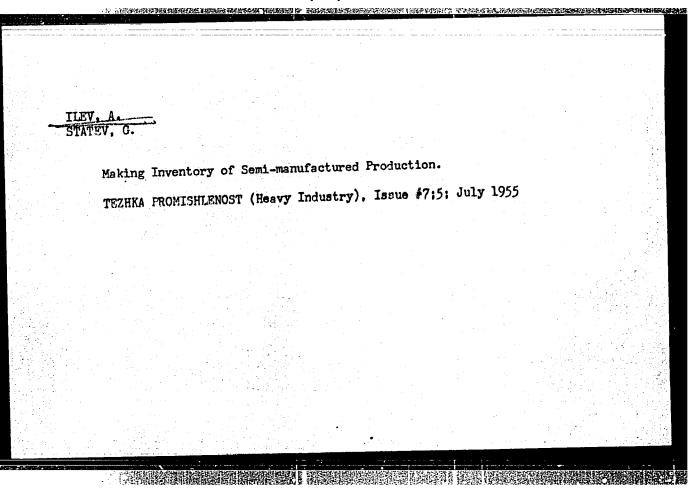
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Ilev, A.; Statev, G. Inventory of unfinished products; experiences of the V. Kolarov High-Voltage Plant. p. 5. TEZHKA PROMISHLENOST. Sofiya. Vol. 4. no. 7. 1955.

SO: Monthly List of East European Accessions, (EEAL), IC. Vol. 4, No. 11, Nov. 1955, Uncl.



ILEV, M.

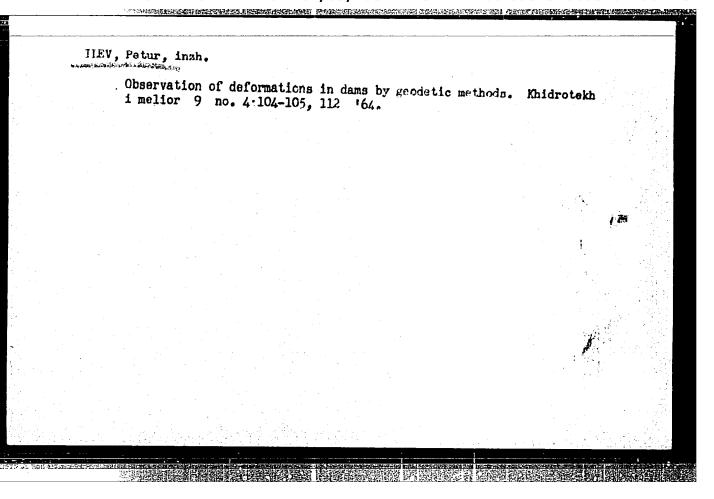
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SO: Monthly List of East European Accessions (EEAL) LC, Vol. 6, no. 12, December 1957 Uncl.

RASCHEEFF, N. [Rascheev, N.]; ILEFF, N. [llev, N.]

Breakage process equation - strain energy factor, and its determination. Doklady BAN 17 no.4:391-393 '64.

BU/2506/66/009/000/0127/0134 SOURCE CODE: ACC NRI AT7005781 AUTHOR: Iley, Nikola; Mikhaylov, Mikhail ORG: none TITLE: An instrument for discrete measurements of elastic body wave propagation velocity SOURCE: Bulgarska akademiya na naukite. Geofizichniya institut. Izvestiya, v. 9, 1966, 127-134 TOPIC TAGS: seismic modeling, elastic wave propagation, earth crust, earthquake, FORWERSTING, WAVE PROPAGATION, LONGITUDINAL WAVE, SEISMOLOGIC ABSTRACT: Schematic diagrams and a description of an instrument designed to measure longitudinal elastic wave velocities are given. Discrete measurements are made that count the number of pulses leaving one generator with a constant repetition frequency and pass through a counter in the time that the elastic wave covers the distance between two observation points. This velocity can be measured with the necessary precision by selecting a suitable base between the observation points and a suitable generator frequency. Owing to its small size and portability, the instrument is well suited for rapidly determining soil layer thickness, investigating low-velocity zones in seismic prospecting and rock pressure in mining operation, geologic mapping, and monitoring changes in the state of the earth's layers in connection with earthquake forecasting.
SUB CODE: 08/ SUBM DATE: 02Dec65 ORIG REF: 006/ [WA-79-67-4] 1/1 Card



ILEVE. P.

SCIENCE

Periodical: IZVESTIIA. BULLETIN Vol. 8, 1957

ILIEV, P. Polyploidy in sesame. p. 3.

Monthly List of East European Accessions (EEAI), IC, Vol. 8, no. 10, 2 February 1959, Unclass.

ZALESKI, V., dotsent; STOYKO, A., veterinarnyy vrach; HEVICH, L.

Propolis in the treatment of wounds in animals. Veterinariia 41 no.2:110-111 F '65. (MIRA 18:3)

1. Silezskaya meditsinskaya akademiya (for Zaleski). 2. Gosudarstvenno-lechebnoye uchrezhdeniye dlya zhivotnykh, Katovitse (for Stoyko).

ZAJUSZ, Kazimierz; ILEWICZ, Leszak; ZALESKI, Władysław

Phosphatases in dental pulp. Part 1. Csas. stomat. 18 no.11: 1277-1283 N * 65.

1. Z Pracowni Patologii Dawiadczalnej Instytutu Medycyny Pracy w Przemysle Weglowym i Hutniczym w Zabrzu (Kierownikz doc. dr. K. Zajusz) oraz z Zakladu Stomatologii Zachowawczej Slaskiej AM (Kierownikz doc. dr. Wl. Zaleski).

ILEYCHEV. P.G., uchitel' Individual assignments to students studying D.I. Mendeleev's periodic system of elements. Khim. v shkole 18 no.5:48-50 S-0 '63.(MIRA 17:1)

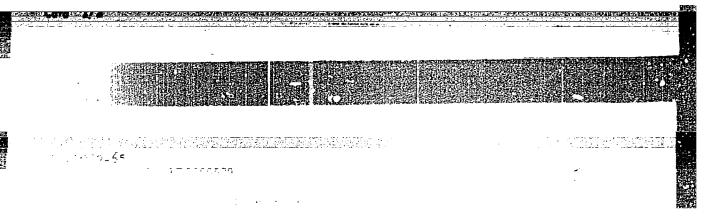
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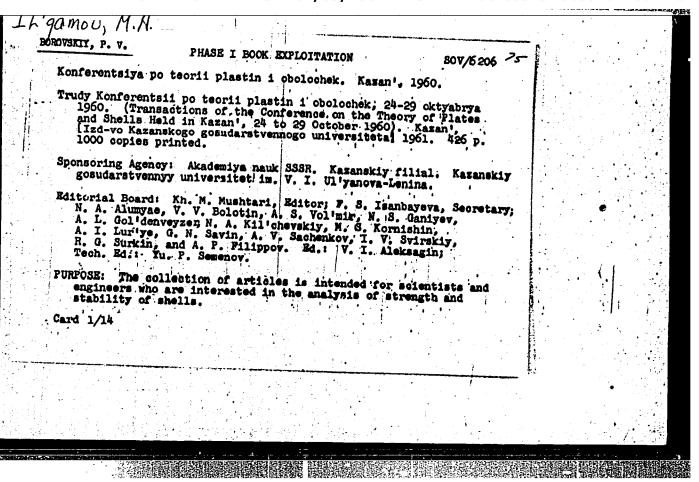
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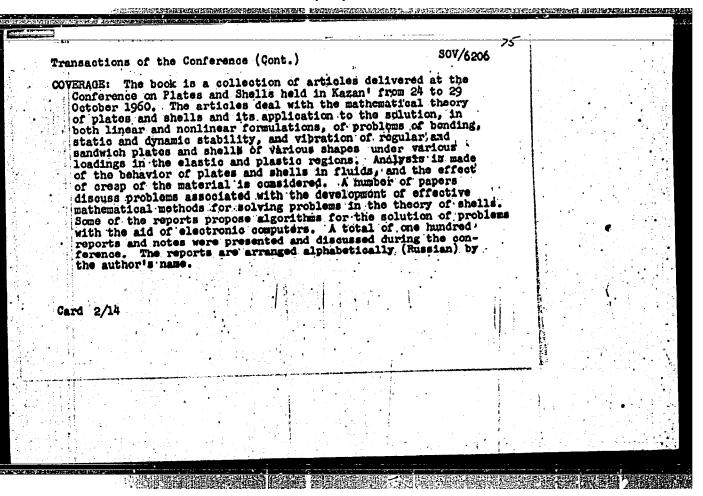
KAMINER, N.S.; ILGACH, S.F.; KHADAKHANOVA, T.S.

Temperature effect of the neutron component of cosmic rays in a period of high solar activity. Geomag. 1 aer. 4 no.5:946-947 S-0 '64. (MIRA 17:11)

1. Institut semnogo magnetisma, ionosfery i rasprostraneniya radiovoln AN SSSR i Irkutskiy gosudarstvennyy universitet imeni Zhdanova.







Transactions of the Conference (Cont.)	SOV/6206	-
Grigorenko, Ya. M. On the Nonsymmetrical State of Stress of a Conical Shell of Linearly Variable Thickness	142	
Dlugach, M. I. Uniqueness Conditions of Displacements in Multiply Connected Regions and Shells With Openings	149	
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Kan, S. N. Thermal Stresses in a Circular Conical Shell	1 164	
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Card 7/14		

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8/124/63/000/004/048/064

AUTHOR:

Il gamov, M. A.

56

TITLE:

Computation of rings for oscillation

PERIODICAL: Referativnyy zhurnal, Mekhanika, no. 4, 1963, 20, abstract 4V157 (Izv. Kazansk. fil. AN SSR. Ser. obshchaya, vyp. 1, 1961, 29-36)

TEXT: The author makes an analysis of free and forced oscillations in rings under the influence of hydrostatic pressure; taking into account the internal resistance of the material and the rotational inertia of the mass of the ring. He adduces general differential equations for plane and spatial oscillations of a circular column, as well as graphics for the relation between natural frequencies of the oscillations and the column of static load; also, of the critical force on the ring as a function of the resilience coefficient of the medium and of the number of waves with loss of stability. The author adduces the data of experiments with a booster fuel collector of a jet engine made in the form of a ring from a pipe. The author computes values for the natural frequencies of bending-torsional oscillations in this ring, taking into account the influence of uniformly distributed jets along the length of the ring, which appear as concentrated masses. He determines the natural frequencies of oscillations of the collector, taking into account fuel pressure. There is a bibliography of four items. Yu. S. Shkenev.

Card 1/1

[Abstracter's note: Complete translation.]

5/147/61/000/004/008/021 E081/E435

10.7500

AUTHOR:

Il'gamov, M.A. (Kazan')

TITLE:

Investigation of forced vibrations of shallow three-ply panels allowing for hysteresis losses in

the filler

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy.

Aviatsionnaya tekhnika / no.4, 1961, 58-65

 λ solution is presented for the problem of determining the TEXT: forced vibrations in a shallow, rectangular, simply supported sandwich panel with asymmetrical structure. The energy dissipation is taken into account only in the core, which is assumed to be absolutely plastic ($E_1 = E_2 = G = 0$), but incompressible along its thickness $(E_3 = \infty)$. The energy loss is measured by the ratio $\psi = \Delta W/W$, where ΔW is the energy dissipated per cycle and W is the energy of vibration. value of ψ for the middle layer (the filler) is large compared with its value for the outer (bearing) layers; for example, in a material with steel bearing layers and a foam filler, the respective ranges of U for the two materials are 0.012 to 0.035 Card 1/2

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Investigation of forced ...

S/147/61/000/004/008/021 E081/E435

and 0.2 to 0.4; the dissipation in the bearing layers can be It is assumed: neglected in comparison with that in the filler. that the dissipative forces causing internal absorption are proportional to the elastic forces but differ in phase from them by a right angle; that the Young's and shear moduli of the filler are zero and that the filler is orthotropic with respect to On this basis, the differential equations of energy dissipation. equilibrium are written down, and the solution expressed as a double trigonometric series for the displacements. characteristic equations are derived and an expression obtained for the amplitude of forced vibrations and for the frequency of natural A numerical example illustrating the calculation of vibration. the amplitude of resonant vibration is given and some experimental tests are briefly described; the logarithmic decrement δ (= $\psi/2$) for a foam filled cantilever beam is measured as lying between the limits 0.12 and 0.2. There is 1 figure.

ASSOCIATION: Kafedra teor. mekhaniki (Department of Theoretical Mechanics)

SUBMITTED: November 18, 1960

Card 2/2

S/879/62/000/000/033/088 D234/D308

AUTHOR: Il'gamov, M. A. (Kazan')

TITLE: Theory of three-layer shells of asymmetric structure

SOURCE: Teoriya plastin i obolochek; trudy II Vsesoyuznoy konfe-

rentell, L'vov, 15-21 sentyabrya 1961 g. Kiev, Izd-vo

AN USSR, 1962, 219-223

TEXT: Using Lagrange's variational equation, the author deduces the equations of motion for orthortropic shells as above, taking into account the deformability of the fillers along the thickness.

Card 1/1.

S/879/62/000/000/040/088 D234/D308

AUTHOR: Il'gamov, M. A. (Kasan')

TITLE: Investigation of forced vibrations of three-layer plates, taking into account hysteresis losses in the filler

SOURCE: Teoriya plastin i obolochek; trudy II Vsesoyuznoy konferentsii, L'vov, 15-21 sentyabrya 1961 g. Kiev, Izd-vo AN USSR, 1962, 260-263

TEXT: The author refers to his previous paper (Izv. AN SSSR, OTN. Mekhanika i mashinostroyeniye, 1961) and quotes the equations of motion given there, substituting

$$G_{13}^{*} = \left(1 + i\frac{\delta_{1}}{\pi}\right)G_{13}, \quad G_{23}^{*} = \left(1 + \frac{\delta_{2}}{\pi}\right)G_{23}, \quad E_{3}^{*} = \left(1 + i\frac{\delta_{3}}{\pi}\right)E_{3}$$
(2)

Card 1/2

Investigation of forced ...

S/879/62/000/000/040/088 D234/D308

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for the displacement moduli of the filler. Deflection amplitudes for the steady state, obtained by the same methods as in the previous paper, are given, together with natural frequencies of skew-symmetrical and symmetrical forms of vibrations.

Card 2/2

39808

5/179/62/000/003/008/015 E191/E435

AUTHOR:

Il'gamov, M.A. (Kazan')

TITLE:

Forced and parametric oscillations of three-ply

sandwich plates

PERIODICAL: Akademiya nauk SSSR. Izvestiya. Otdeleniye tekhnicheskikh nauk. Mekhanika i mashinostroyeniye,

no.3, 1962, 114-119

The problems treated are: three-ply sandwich plates of nonsymmetrical construction with a light-weight core subject to periodic loads arbitrarily distributed over the surfaces of the load carrying face layers; oscillation of sandwich plates of symmetrical construction under the action of forces in the plane V.V.Bolotin has shown (Izv. AN SSSR, OTN, no.4, of the plate. 1956) that, in the case of elastic systems in which the frequencies of longitudinal and flexural oscillations can approach each other, it is necessary to consider simultaneously the longitudinal (non-excited) and the parametrically excited The basic results, when taking into account the non-excited motion, are the discovery of the possible build-up Card/1/

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S/179/62/000/003/008/015 E191/E435

Forced and parametric ...

of parametric oscillations near the resonance of forced oscillations and the widening of the instability regions of the system. Owing to the separation of the load carrying face layers, the ratio of the bending stiffness to the stiffness in extension and compression in three-ply plates is several times larger than the same ratio in single-ply plates so that the two natural frequencies mentioned above may easily approach each other. The plates considered are freely supported along all edges and are loaded by periodic transverse distributed loads. The starting point of the analysis is the variational principle of Lagrange, In the derivation, a linear law is assumed for the deformation of the core in relation to thickness. The analysis shows that, when the periodic load distributions of the two faces are unequal and the phase shift between them is arbitrary and also when the geometric and mechanical properties of the load carrying faces are unequal, the escillations of the plate consist of transverse oscillations superimposed on extension and compression along the thickness. A special case is considered when the oscillations can be split into symmetrical and skew-symmetrical modes. Card 2/3

S/179/62/000/003/008/015
Forced and parametric ...

Second problem considered concerns the oscillation of an infinitely long symmetrically constructed three-ply plate under the action of periodically varying compressive forces. The stability of the non-excited motion is examined. It is shown that taking account of the non-excited motion widens the main region of instability several times, in one numerical example by a factor of 3.

SUBMITTED: September 11, 1961

Card 3/3

ACCESSION NR: AP4033041

8/0147/64/000/001/0060/0066

AUTHOR: Il'gamov, M.A.

TITLE: Non-stationary thermal conductivity and optimal parameters of three-

SOURCE: IVUZ. Aviatsionnaya tekhnika, no. 1, 1964, 60-66

TOPIC TAGS: thermal conductivity, lamina, shell, thermal insulation, heat capacity, deformation, deformation theory, convection, heat transfer

ABSTRACT: In a brief introductory statement the author describes the structure of three-layer laminas and shells and reviews certain of their more salient properties. The contents of some seven articles on this general subject by other authors, whose papers are listed in the bibliography at the end of the paper, are outlined and their pertinence to the general problem area under consideration is indicated. In the present article, the author considered non-stationary thermal conductivity in a lamina consisting of thin outer layers and a thermo-insulated filler. By a thermally thin layer is here to be understood a layer, throughout the thickness of which the temperature is rapidly equalized, with the order of thickness being determined on the basis of the Card 1/4

ASSESSION NR: Ap4033041

criterion of skin thinness. The effect of the thin outer layers on the heating process of the lamina is evaluated by the thermal capacitances C' and C", of these layers which equal $C' = 2c'\gamma'h'$, $C'' = 2c'\gamma''h''$, (1)

where c',c",y', y" are the specific thermocapacitances and densities of the materials of the outer layers. Heat radiation from free surfaces and changes in the thermo-physical properties of the layers during heating are disregarded. The nomenclature and the coordinate system used in the paper were borrowed from the theory of deformations of three-layer laminas and shells. The author considered the heating of such a lamina with thermo-insulated borders, the original temperature of which was To = const. with convective heat transfer. Equations are derived for determining the temperatures of the layers, and the point is made that, knowing these layer temperatures, the thermo-physical properties corresponding to them can be found and on this basis the temperature distribution in the second approximation can be determined. A numerical example is given for a lamina consisting of steel and aluminum outer layers and a plastic filler of specific geometrical and physical parameters. The next question considered by the author is that of selecting the optimal thicknesses for the

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ACCESSION NR: AP4033041

carrying layers of a freely-supported, three-layer lamina of non-symmetrical structure during its heating. For the sake of simplicity, a lamina of infinite length is considered. A determination is made of the ratios of the thicknesses of the carrying layers to the overall thickness of the lamina, resulting in minimal lamina weight with prescribed strength D (for time t). The following formula for strength is derived:

$$D = \frac{\int_{0}^{\zeta_{1}} \frac{n^{2}/2H}{n^{2}}}{\frac{n^{2}}{G} + (1 + \zeta' + \zeta'') \left(\frac{1}{E'\zeta'} + \frac{1}{E''\zeta''}\right)}.$$
 (2)

while the weight of a lamina of unit length will be:

$$P = 2l(\gamma'h' + \gamma h + \gamma''h'') = 2lH[(\gamma' - \gamma)\zeta' + (\gamma'' - \gamma)\zeta'' + \gamma].$$
 (3)

The condition for the relative minimum has the form:

$$\frac{\partial D}{\partial C} \frac{\partial P}{\partial C} - \frac{\partial P}{\partial C} \frac{\partial D}{\partial C} = 0,$$
 (4)

Card 3/4